

# The Contribution of Rubber Adhesion to Sealability at Deep Freeze Temperatures

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1

Purpose

2

Factors impacting vial stopper sealability

3

Understanding of rubber adhesion at temperatures below glass transition temperature ( $T_g$ )

- Literature search
- Testing

4

Takeaways

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Future work

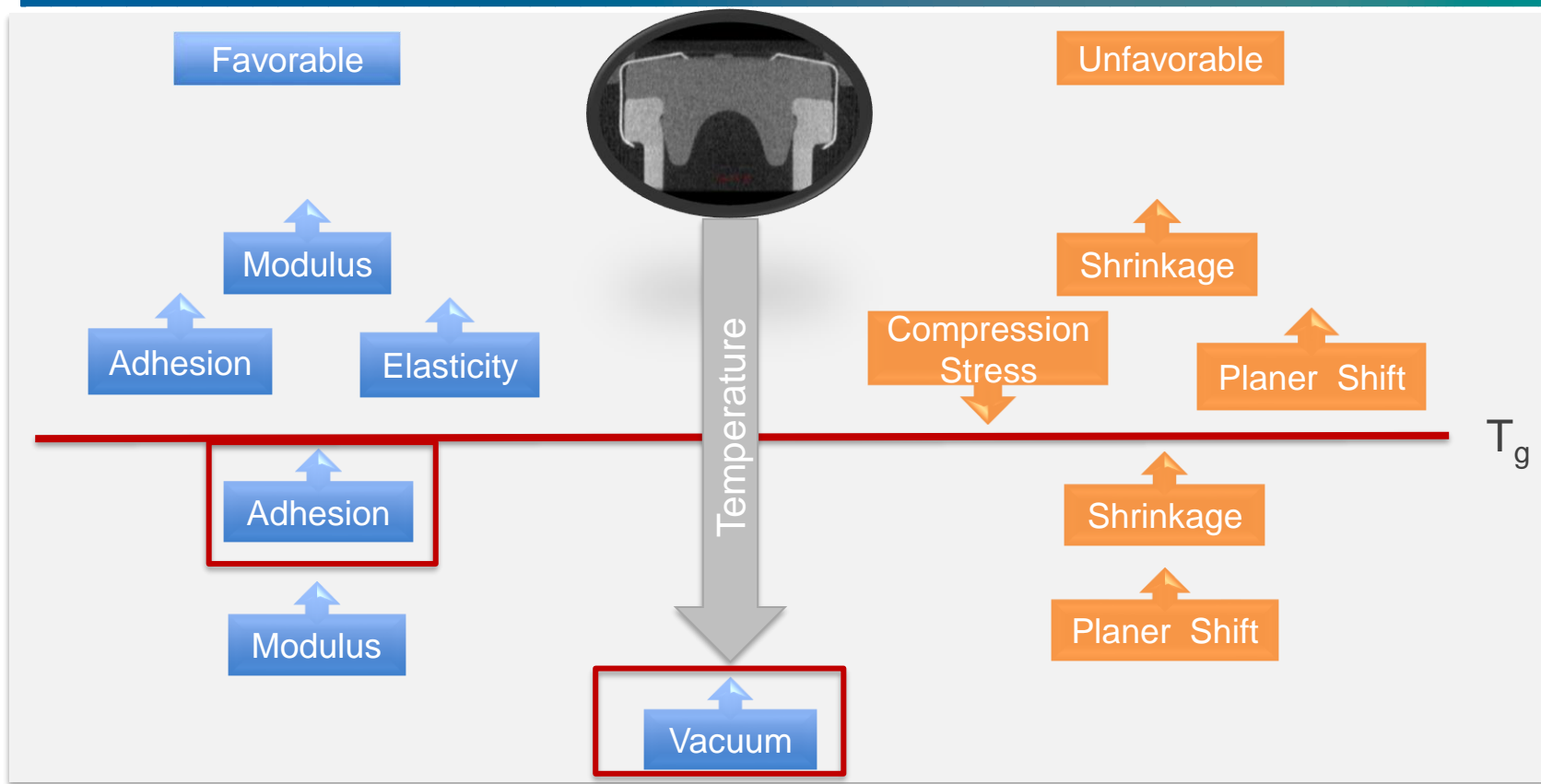
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Acknowledgements

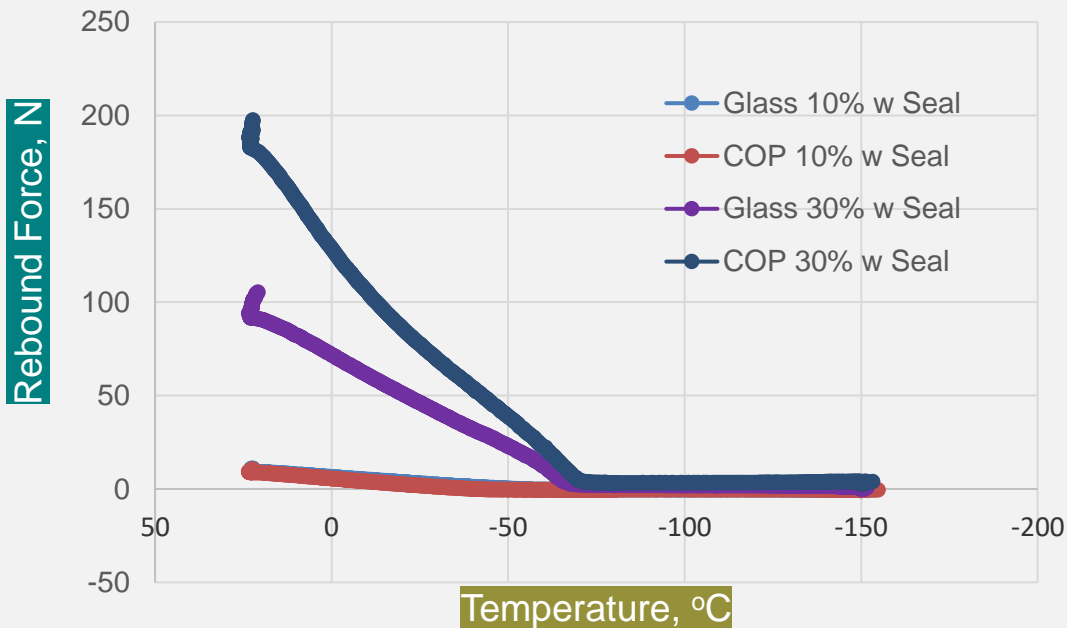
- Elasticity above & below  $T_g$
- What makes rubber seal at temperatures below  $T_g$ ?
- Shrinkage above & below  $T_g$
- Does polymer chain co-mingling occur between rubber and COC/COP vials?
- The lower the  $T_g$ , the better sealability at low temperatures?



COC – cyclic co-polymer; COP – cyclic polymer.



Stopper Rebound Force with Temperature By DMA



DMA Testing conditions:  
 Compression: 10% & 30%  
 1) Isothermal for 1hr @ RT  
 2) Cool to -80°C at 1°C/min  
 3) Cool to -150°C at 10°C/min



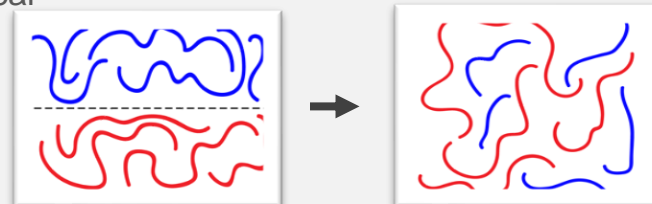
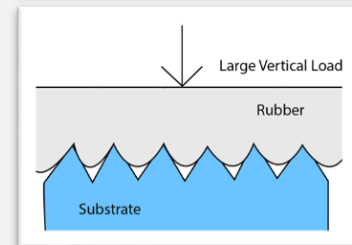
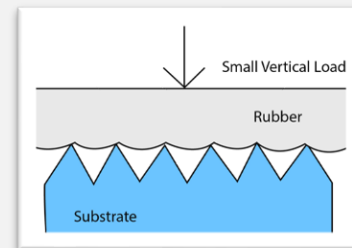
DMA – Dynamic Mechanical Analysis

## Coefficient of Linear Thermal Expansion (CLTE)

<u>SAMPLE</u>	<u><math>T_g</math> by DMA, °C</u>	<u><math>\frac{CLTE (/\text{°C}) \times 10^{-6}}{T_g - 125 \text{ °C}}</math></u>	<u><math>\frac{CLTE (/\text{°C}) \times 10^{-6}}{-120 \text{ °C} - T_g}</math></u>
Rubber 1	-55	293.7	74.1
Rubber 2	-86	305.6	89.87
Rubber 3	-55	221.7	62.84
Rubber 4	-55	222.0	65.10

- Rubber shrinkage varies with formulations.
- The shrinkage is much higher above  $T_g$  than below  $T_g$ .
- $T_g$  and CLTE do not have direct correlation.

- Physical adsorption – intermolecular interactions with intimate contact
  - Wettability
  - COC/COP vs glass with rubber
- Mechanical adhesion – interlocking surfaces by filling voids and pores of surfaces
  - Contact area: surface roughness, pressure, viscosity...
- Diffusion – merge at interface by diffusion
  - molecules mobile and soluble, oil in thermoplastic elastomer (TPE)
  - polymer chains ends inter-penetration at interface
  - contact time, temperature, molecular weight, physical forms...
- Chemical bonding
- Electrostatic

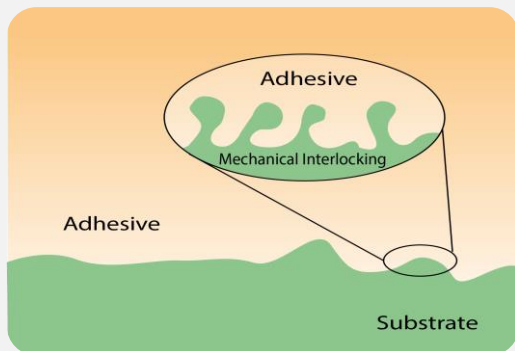


<sup>1</sup> Adapted from: S Athavale, Adhesion and Must be cited as: Adhesives Theory presentation, September 10, 2010, SIES College of Arts, Science & Commerce, Nerul, Navi Mumbai, India.

## General Adhesive

Two steps to achieve adhesion:

- Wetting
- Solidification

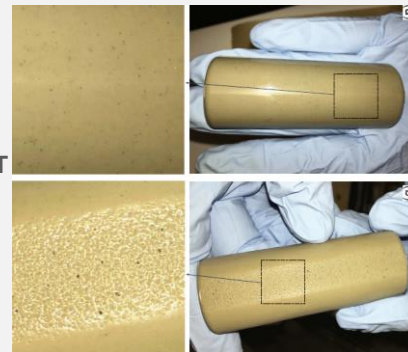


## Rubber Adhesion<sup>2</sup>

Two steps to achieve adhesion:

- Close contact under pressure
- Chain frozen at  $T_g$

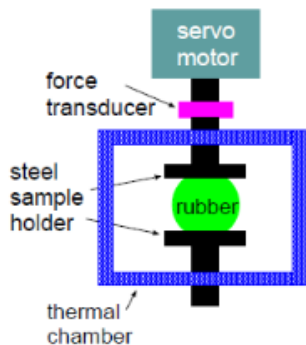
HNBR  $T_g$  -16°C  
10-20% CS @ RT  
On PMMA  
Cooled to -40°C



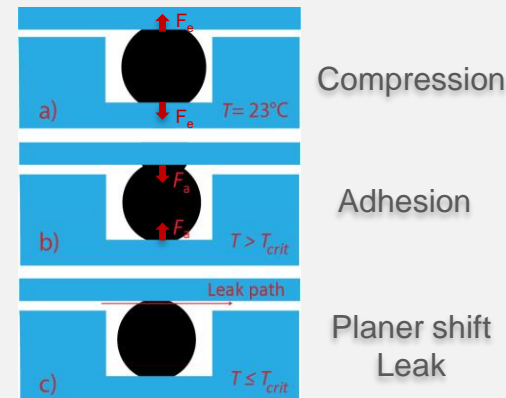
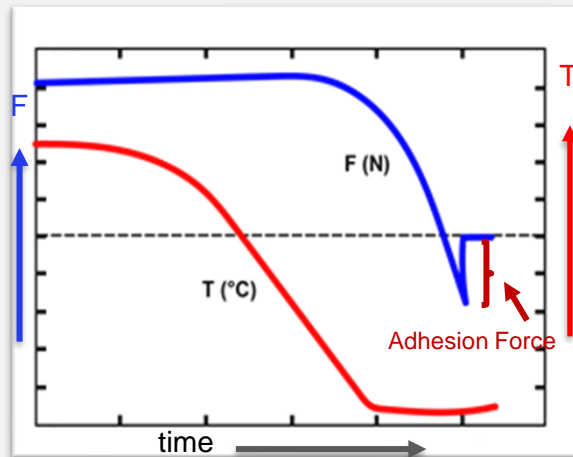
HNBR - Hydrogenated Nitrile Butadiene Rubber; CS – compression strain; RT – room temperature.

<sup>2</sup> AG Akulichiev, A Tiwari, L Dorogin, AT Echtermeyer and BNJ Persson. Rubber adhesion below the glass transition temperature: Role of frozen-in elastic deformation. EPL, 120 3 (2017) 36002.





**DMA** - Initial compression strain 10% at RT, cooled down to -50°C.



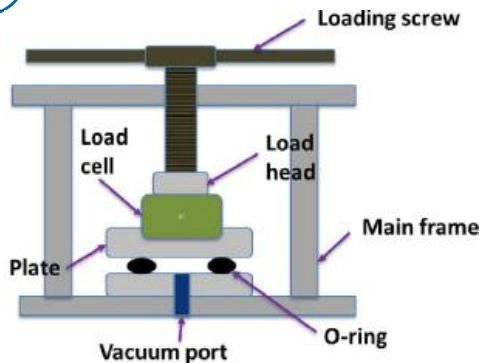
Two different math equations of adhesion force:  $T > T_g$  and  $T < T_g$



$T > T_g$ : JKR (Johnson-Kendel-Roberts) Theory

$$f_c = - \frac{3\pi E_0^* a_c^2}{4R}$$

$$T < T_g: f_{\text{pull-off}} \approx (2\pi\omega a E_1^*)^{1/2}$$



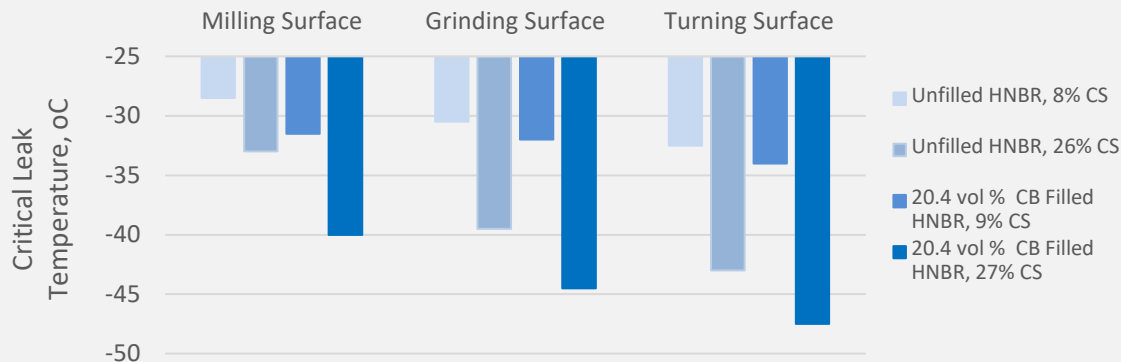
**HNBR:** non-filled and 20.4% CB filled

**Compression:** 7% & 30%

**Sealing surface:** milling, grinding & turning

**T<sub>g</sub>:** ~-16°C (DMA), -23°C (DSC)

**Vacuum:** 100 kPa



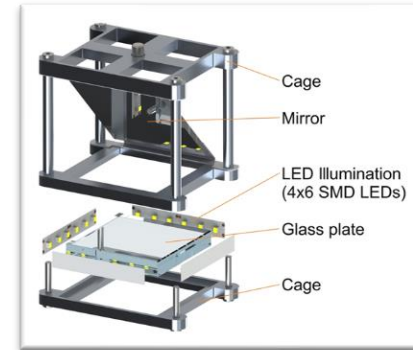
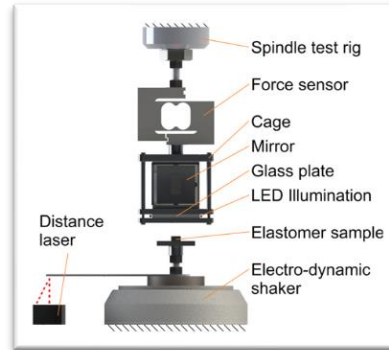
Rubber seal leak temperature depends on adhesion force, which depends on:

- rubber formulation
- sealing surface topography and
- compression

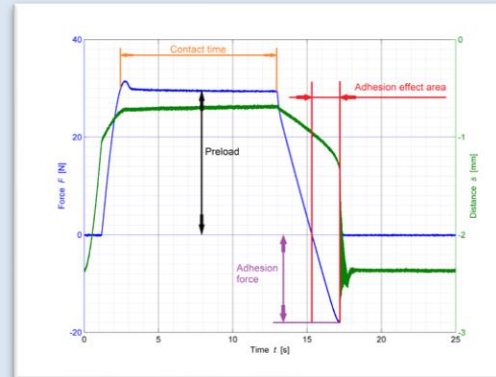
$$\Delta T_{adh} = \frac{f_{adh}}{2aE\alpha}$$

<sup>3</sup> Data and image adapted from: AG Akulichova, AT Echtermeyer, BNJ Persson, Interfacial leakage of elastomer seals at low temperatures, International Journal of Pressure Vessels and Piping, 160 2018 (14-23).

## Adhesion Test Rig



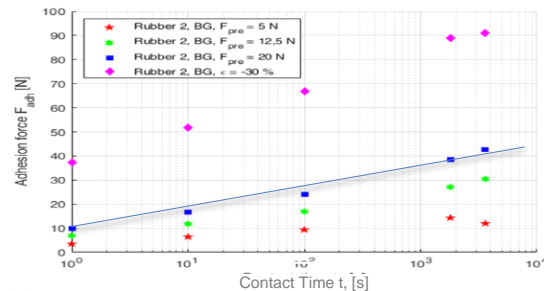
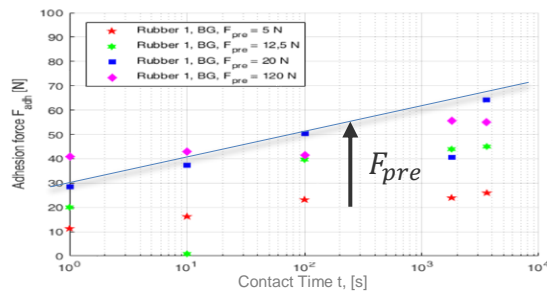
## Adhesion Force & Visualization



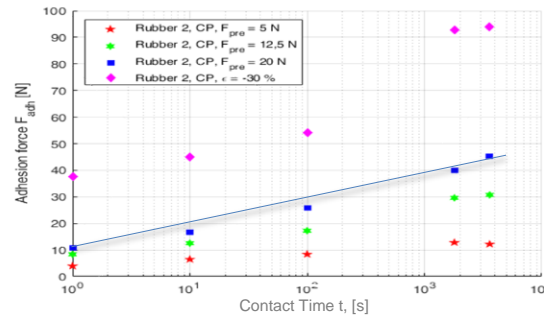
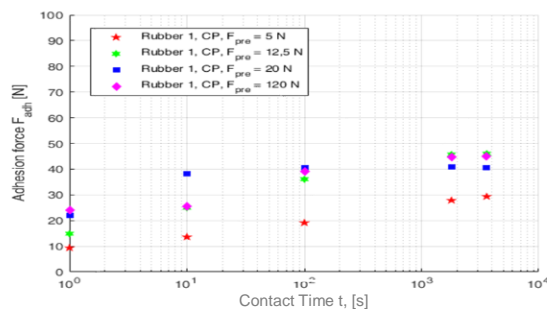
## Rubber 1

## Rubber 2

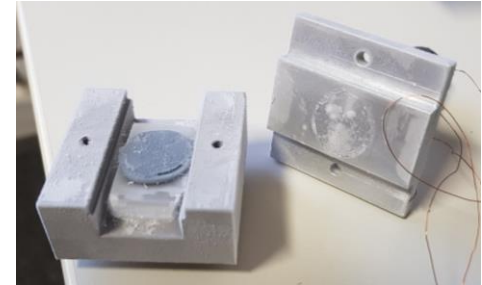
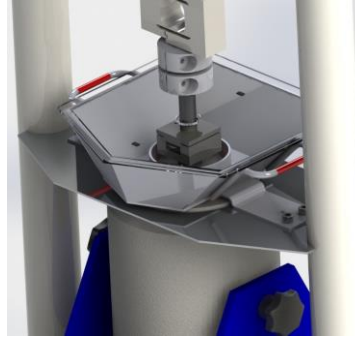
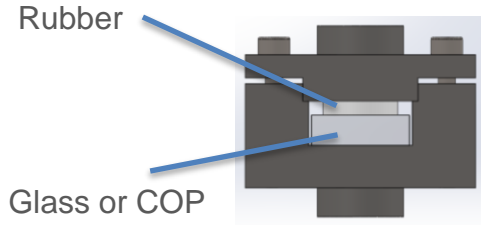
Glass



COP



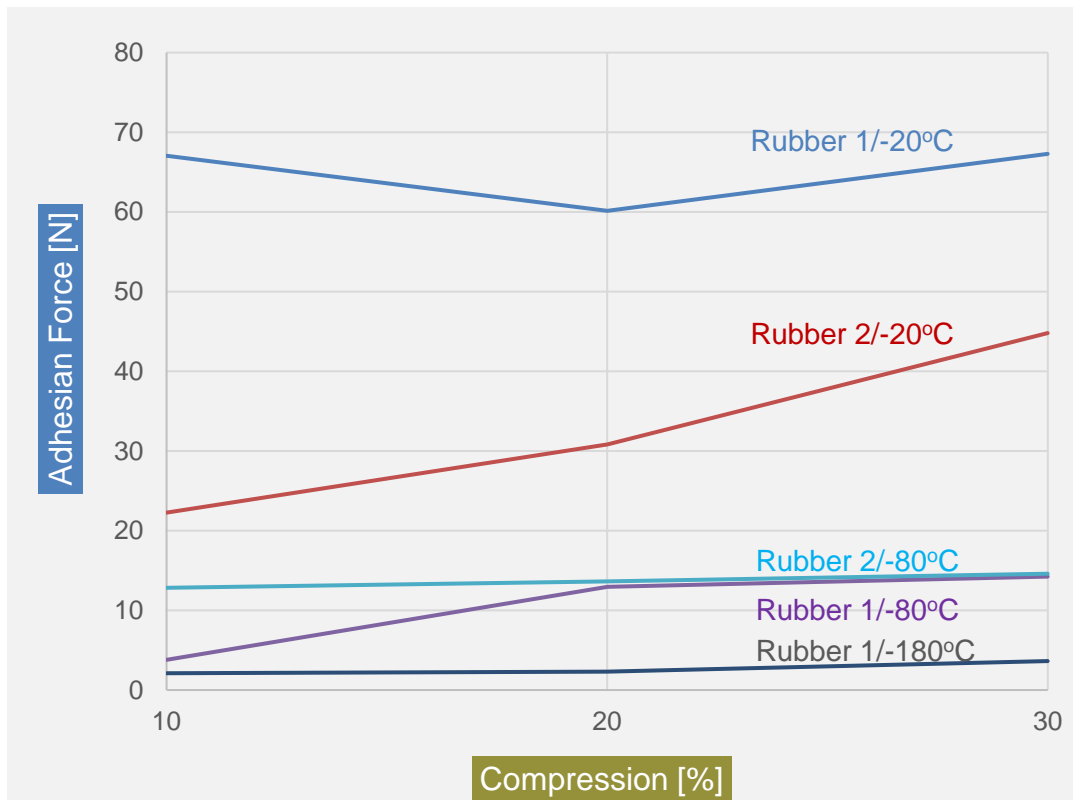
- Adhesion force is rubber formulation-dependent.



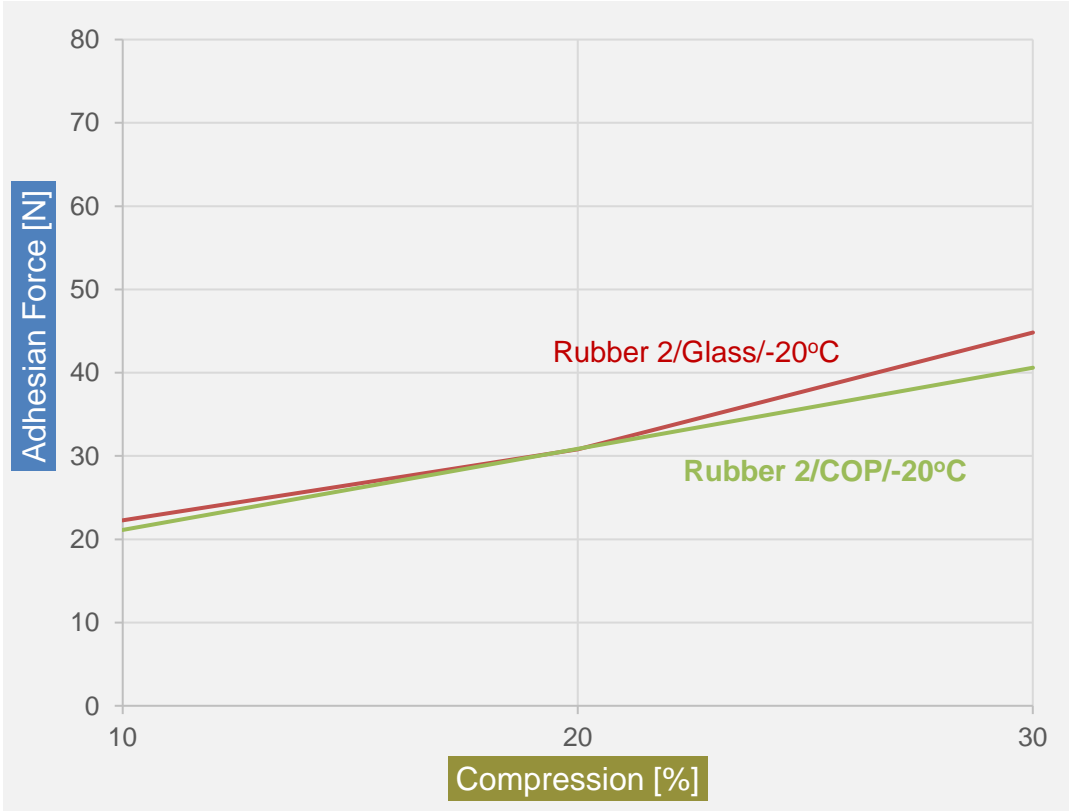
- Equipment limitation
- Time to equilibrium  $\geq$  4hours

- Ice generation
  - $N_2$  vapor
  - mold design

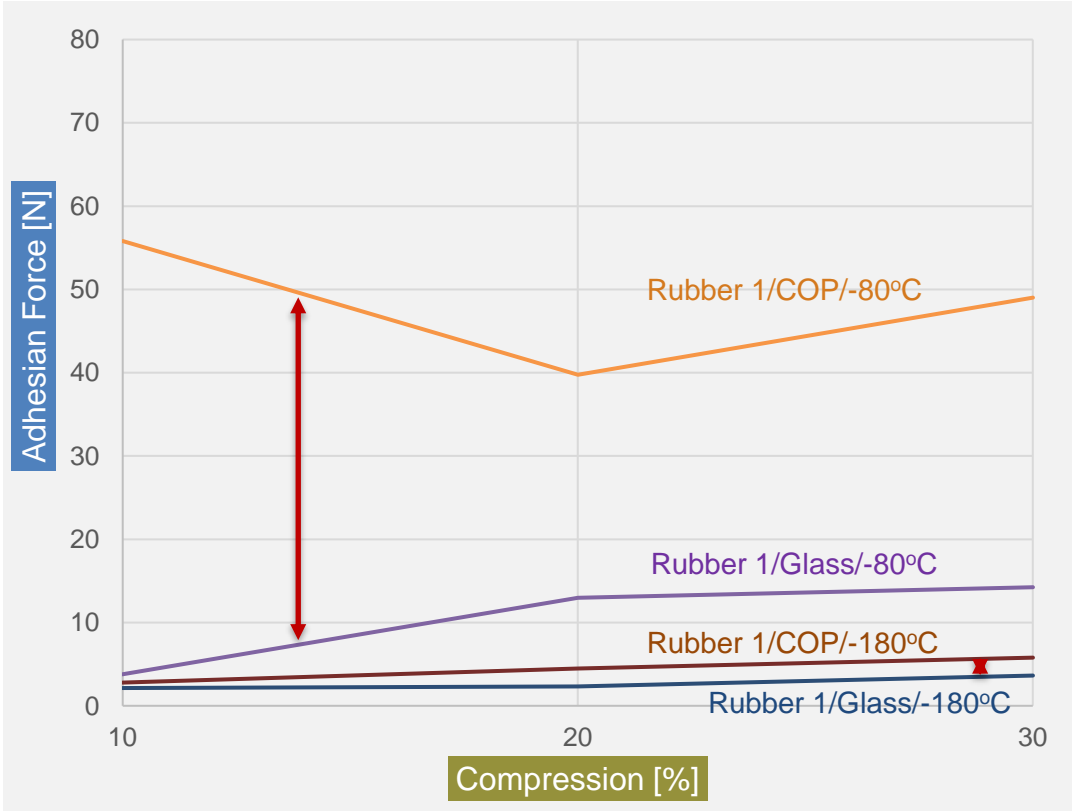
- Glue failure
  - steel & COP
  - steel & rubber



- Adhesion force to glass decreases with temperature for both rubbers.
- At 10% - 30% compression, no separation between rubber and glass occurred.

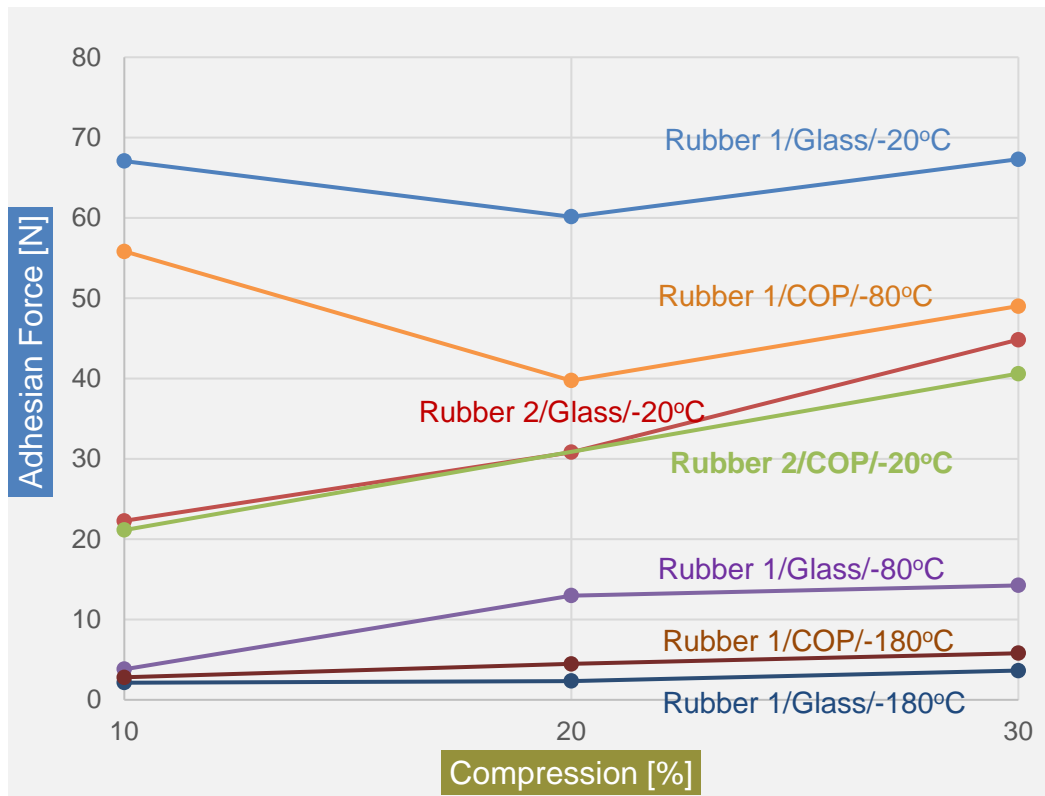


- The adhesion behavior of Rubber 2 at -20°C is similar to room temperature.



- Adhesion of Rubber 1 with COP is stronger than with glass at temperature below  $T_g$ .
- Rubber 1 generates additional adhesion with COP at temperature below  $T_g$ .





- Adhesion of Rubber 1 with COP is stronger than with glass at temperature below  $T_g$ .
- Rubber 1 generates additional adhesion with COP at temperature below  $T_g$ .

1

Adhesion becomes the major sealing force at temperatures below  $T_g$ .

2

Mechanical adhesion generates at  $T_g$ , determined by rubber formulation, matrix material, surface roughness and compression pressure.

3

Rubber shrinkage is much higher at temperatures above  $T_g$  than below  $T_g$ .

1

Test adhesion of CCS system at room temperature vs low temperature.

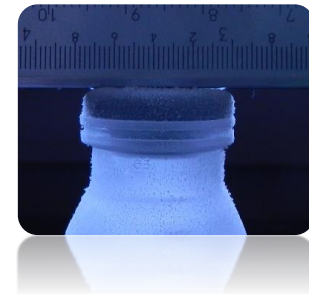
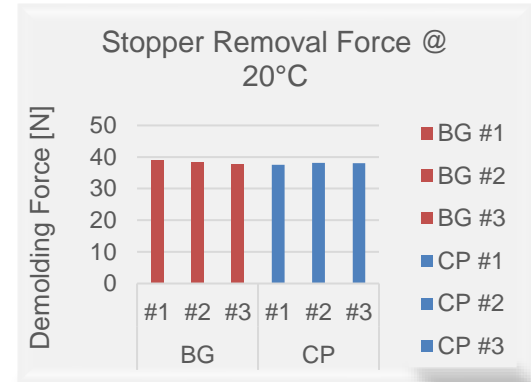
- Design
- Surface
- Lubrication
- Vacuum

2

Explore math modeling to predict leak temperature.

- Adhesion limit correlation with leak

CCS – Container Closure System



# Acknowledgements

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